MULTIPLIERLESS TWO-CHANNEL PERFECT RECONSTRUCTION LATTICE FILTER BANK DESIGN USING SPECTRAL FACTOR SELECTION

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A two-channel perfect reconstruction lattice filter bank proposed in [1] is considered. We have assumed that involvement of a spectral factor selection into multiplierless lattice filter bank design algorithms can improve results. It is confirmed by the design example at nominal edges $f_{1n}=0.18$, $f_{2n}=0.32$ and the sampling frequency equal 1. We used two algorithms based on a variation of initial parameters (VIP) as [4]. The results [2-4] may be improved by using a special spectral factor. That is shown in Table1. Here 2N-1 is the order of each filter in the bank; C is the spectral factor code; M is the fractional part wordlength of coefficients; m is the number of non-zero bits in coefficients; f_1 and r are the passband edge and auxiliary parameter [4] for which the solution is obtained; \tilde{a}_0 - the minimum stopband attenuation; Σ - the total number of adders including the structure adders (first item) and adders (second item) replacing all pairs of multipliers on coefficients α_1 in Fig.1b in [2,3].

| | | | | | | | Table 1 |
|---------------------------|------|----|----|-----|----------------|---------------------------|------------------------|
| Algorithm | 2N-1 | С | Μ | m | $f_1; r$ | $\widetilde{a}_0^{}$, dB | Σ |
| Simple rounding [2] | 27 | | 10 | 2 | - | 25.38 | 56=28+14×2 |
| Tree search [2] | | 0 | | | - | 45.37* | 56=28+14×2 |
| Implicit enumeration [3] | 21 | | 9 | ≤ 3 | - | 45.19* | 56=22+17×2 |
| VIP [4] | | | | | 0.18053; 3 | 45.01 | 56=22+17×2 |
| | | 0 | 10 | | 0.1950; 0.1683 | 38.85 | 52=28+12×2 |
| VIP | | 33 | 8 | | 0.1788; 0.1367 | 46.79 | 54=28+13×2 |
| | | | 7 | | 0.1794; 0.1429 | 44.06 | 50=28+11×2 |
| | 27 | 0 | | | 0.1780; 0.4398 | 40.98 | 50=28+11×2 |
| VIP + variation of | | | 10 | ≤2 | 0.1788; 0.1367 | 48.10 | 56=28+14×2 |
| coefficients (coordinate- | | 33 | | | 0.1800; 0.1481 | 47.81 | 54=28+13×2 |
| wise search) | | | 7 | | 0.1786; 0.1377 | 46.08 | 50=28+11×2 |
| | | | | | 0.1810; 0.1600 | 44.38 | $44 = 28 + 8 \times 2$ |

In case C=0 the passband zeros of the transfer function are $R_6 \exp(\pm j\varphi_6)$, $R_5 \exp(\pm j\varphi_5)$, ..., $R_1 \exp(\pm j\varphi_1)$, R_0 and in case C=33 the zeros are $R_6 \exp(\pm \varphi_6)$, $R_5^{-1} \exp(\pm \varphi_5)$, $R_4 \exp(\pm \varphi_4)$, ..., $R_1 \exp(\pm \varphi_1)$, R_0^{-1} . Here R_i is the radius and φ_i is the angle of i-th zero in z-plane. In addition $R_i < 1$, i=0,1,...,6 and $\varphi_1 < \varphi_2 < ... < \varphi_6$. For the solution with $\tilde{a}_0 = 48.10$ dB the coefficients are α_0 ,..., α_{13} : $-2 + 2^{-3}$, $2^{-1} + 2^{-7}$, $2^{-1} + 2^{-5}$, $2^{-5} - 2^{-8}$, $2^{-1} + 2^{-6}$, $2^3 - 1$, $-2^{-1} - 2^{-7}$, $2^{-2} - 2^{-6}$, $1 - 2^{-7}$, $-2^{-6} + 2^{-8}$, $-2^{-3} + 2^{-5}$, $2^{-3} + 2^{-6}$, $-2^{-4} + 2^{-6}$, $2^{-6} - 2^{-10}$. For the solution with $\tilde{a}_0 = 46.08$ dB all coefficients are identical except $\alpha_3, \alpha_9, \alpha_{13}$: $2^{-5}, -2^{-6}, 2^{-6}$. It is interesting that the solution with $\tilde{a}_0 = 46.79$ dB differs from the one with $\tilde{a}_0 = 48.10$ dB by the only coefficients from [2,3].

References

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